Independent Geometrical Control of Spin and Charge Resistances in Curved Spintronics

Kumar Sourav Das,*† Denys Makarov,‡ Paola Gentile,§,○ Mario Cuoco,§,○ Bart J. van Wees,† Carmine Ortix,†,||,‡* and Ivan J. Vera-Marin*†

†Physics of Nanodevices, Zernike Institute for Advanced Materials, University of Groningen, 9747 AG Groningen, The Netherlands
‡Helmholtz-Zentrum Dresden-Rossendorf, Institute of Ion Beam Physics and Materials Research, Bautzner Landstrasse 400, 01328 Dresden, Germany
§CNR-SPIN, c/o Università degli Studi di Salerno, I-84084 Fisciano, Italy
| Dipartimento di Fisica “E. R. Caianiello”, Università degli Studi di Salerno, I-84084 Fisciano, Italy
| ‡Institute for Theoretical Physics, Center for Extreme Matter and Emergent Phenomena, Utrecht University, Princetonplein 5, 3584 CC Utrecht, The Netherlands
| §Institute for Theoretical Solid State Physics, IFW Dresden, 01171 Dresden, Germany
| ○School of Physics and Astronomy, University of Manchester, Manchester M13 9PL, United Kingdom

Supporting Information

ABSTRACT: Spintronic devices operating with pure spin currents represent a new paradigm in nanoelectronics, with a higher energy efficiency and lower dissipation as compared to charge currents. This technology, however, will be viable only if the amount of spin current diffusing in a nanochannel can be tuned on demand while guaranteeing electrical compatibility with other device elements, to which it should be integrated in high-density three-dimensional architectures. Here, we address these two crucial milestones and demonstrate that pure spin currents can effectively propagate in metallic nanochannels with a three-dimensional curved geometry. Remarkably, the geometric design of the nanochannels can be used to reach an independent tuning of spin transport and charge transport characteristics. These results laid the foundation for the design of efficient pure spin current-based electronics, which can be integrated in complex three-dimensional architectures.

KEYWORDS: Spintronics, nonlocal spin valves, curved nanoarchitectures, geometrical control, electrical and spin resistance

A number of next-generation electronic devices, including memory elements and transistor circuits, rely on spin currents. Pure spin currents1–7 transfer only spin angular momentum and therefore have the additional advantage that the electronic devices can operate with a low power dissipation. A pure spin current can be generated using the coupling between charge and spin transport across the interface of a ferromagnet with a contiguous paramagnetic nanochannel. The efficiency of the spin injection across this interface can be optimized by improving the interface quality and the device structure. The propagation of the pure spin current along the nanochannel is instead related to its spin relaxation length. In conventional metals and small-gap semiconductors, the dominant spin relaxation mechanism corresponds to the so-called Elliot–Yafet mechanism,8,9 which dictates that the spin relaxation length is strictly locked to the resistivity of the metallic paramagnet. This, in turn, severely compromises the applicability of pure spin currents to technologically relevant modern electronics, which necessitates the individual matching of spin and charge resistances in order to achieve efficient coupling of spin and charge degrees of freedom.8,10,11

Here, by using a combination of experimental investigations and theoretical analysis, we show that spin and charge resistances can be independently tuned in metallic nanochannels. Importantly, this is realized even in the absence of any external electric or magnetic gating,12,13 and it is totally different in nature to the spin-charge separation phenomenon in Tomonaga–Luttinger liquids.14,15 Our strategy relies on the possibility to grow metallic nanochannels with a strongly inhomogeneous nanometer-scale thickness, t. The size-dependent resistivity, ρ, of the metallic channels16 yields a different local behavior for the sheet resistance ρ/t and the spin relaxation length λ ∝ 1/ρ [c.f. Figure 1a–c]. As a result, an appropriate engineering of the nanochannel thickness allows for designed nanochannels, where one can achieve independ-
ent tuning of the spin resistance without affecting the total charge resistance, and vice versa. This capability allows for the design of an element with simultaneous matching of spin resistance to a spin-based circuit, e.g., for efficient spin injection,10,11 and matching of charge resistance to a charge-based circuit, e.g., for efficient power transfer. The control of spin and charge resistances is fundamental to spintronics, as it enables practical magnetoresistance in two terminal devices17 and the concatenability and reduced feedback in spin logic architectures.18,19

As a proof of concept, we demonstrate modulation of spin currents and of charge currents in lateral nonlocal spin valves2 with ultrathin metallic channels directly grown on curved templates [c.f. Figure 1d,e], thereby allowing us to achieve efficient spin current propagation in three-dimensional nanoarchitectures. This is of immediate relevance when considering a practical implementation of spintronics. On the one hand, the transport of pure spin currents in nonlocal spin valves is at the heart of multiple proposals of spin-based logic architectures,18,19 and thus of potential technological impact. On the other hand, the use of curvature to independently control spin and charge impedances in multiterminal devices adds a novel approach for their efficient integration with complementary metal oxide semiconductor (CMOS) transistors that optimizes device reliability and endurance.20 Finally, as CMOS technology scales down to 10 nm features or less, there are increasing efforts in the development of three-dimensional CMOS microelectronics that can overcome the limitations of Moore’s law. This is similar to spintronics and its integration with CMOS. Such efforts have been led by the thinning and 3D stacking of several chips, initially integrating CMOS and spin-based memories21 and later extended to heterogeneous chips.22 A completely different approach is to change the architecture itself to be three-dimensional. Until now, the realization of vertical flow of spin information via three-dimensional channels has been based solely on the movement of magnetic domain walls, by applying a current or magnetic field,23 with a recent implementation based on depositing magnetic material on the side-wall of deep trenches.25

Our work on curved nanoarchitectures for pure spin current devices delves into territory so far only explored for charge-based technologies. While being conceptually simple and potentially cheap, it offers the possibility of high-density three-dimensional integration over that in conventional spin current devices.

Curved templates were created in the form of trenches in a silicon dioxide substrate. Increasing the height of the trenches, A [c.f. Figure 1d,e], led to channels with increasing curvature, allowing us to systematically explore the effect of channel geometry. To create the trenches, we used focused ion beam (FIB) etching, where the geometry of the trenches was controlled by varying the FIB milling times. Each sample consists of two lateral spin valve devices: one device with the spin transport channel across the trench, resulting in a curved device, and another on the flat part of the substrate, serving as a reference device. The spin valve devices were prepared by multistep e-beam lithography, e-beam evaporation of materials, and resist lift-off techniques, as described.26 Permalloy (Ni$_{80}$Fe$_{20}$, Py) nanowires, with a thickness of 20 nm, were used as the ferromagnetic electrodes. Injector and detector Py electrodes were designed with different widths (80 and 100 nm) to achieve different coercive fields. The injector-detector in-plane separation (L) was 500 nm for all of the devices, except for the one with the largest trench height (A = 270 nm), which had a separation of 700 nm. For the spin transport channel, we used a Py/Pt layer, with a width of 100 nm and a nominal thickness of 50 nm. The Al channel was evaporated following a short in situ ion milling step to remove surface oxide and resist contamination from the Py electrodes, resulting in Al/Pt ohmic contacts with a resistance-area product lower than $10^{-15}$ Ω m$^2$. Figure 1f shows a scanning
electron microscope image of one of the fabricated curved spin valve devices.

All electrical measurements were performed with the sample in a high vacuum environment, within a liquid helium cryostat. The electrical resistance of the Al channel was measured by the four-probe method, with the current applied between the two ends of the Al channel and the voltage drop measured between the injector and the detector electrodes. For the nonlocal spin valve measurements, the electrical connections are schematically shown in Figure 1f. Here, an alternating current (I) source, with a magnitude of 400 μA and frequency of 13 Hz, was connected between the injector electrode and the left end of the Al channel. The nonlocal voltage (V) at the detector electrode, with reference to the right end of the Al channel, was measured by a phase sensitive lock-in technique. A magnetic field was applied along the length of the Py wires during these measurements to configure the injector and detector electrodes in a parallel (P) or an antiparallel (AP) state, corresponding to two distinct levels of the nonlocal resistance (R\text{NL} = V/I). The spin valve signal (ΔR\text{NL}) is then given by the difference of the nonlocal resistance between parallel and antiparallel configurations, ΔR\text{NL} = R\text{NL}^P - R\text{NL}^AP. The measurements were carried out at room temperature and at 4.2 K to study spin transport in channels with increasing curvature. The extraction of ΔR\text{NL} via this standard low-frequency first-harmonic lock-in technique serves to accurately extract the pure spin current signal and exclude any role of induction or thermoelectric effects.1,2,6

The nonlocal spin valve measurements are shown in Figure 2a. The resulting modulation of ΔR\text{NL} with A is plotted in Figure 2b. ΔR\text{NL} is the maximum for the reference spin valves with A = 0 and shows little change for trenches with A < 50 nm, limited by device to device variation. However, for increasing trench heights above ≈100 nm, we observe a strong decrease in ΔR\text{NL}, until it is fully suppressed for the trench with A = 270 nm. On the other hand, the measured four-probe charge resistance of the curved channel between the injector and detector electrodes exhibited an opposite trend, as observed in Figure 2c. Here, a steep increase in resistance (R) is seen for trenches with a height greater than ≈100 nm. A similar behavior was observed at room temperature [see Supporting Information, section 1].

The contrasting behaviors of both the spin valve signal and charge resistance offer direct evidence of the effect of the curved geometry introduced by the trench. We have first checked that both the strong suppression of ΔR\text{NL} and the steep increase of R with increasing A cannot be explained just by considering the increase in the channel length due to the curved geometry. To properly describe both of these behaviors, we have therefore developed a theoretical model, which is applicable to devices, where the local channel geometry explicitly impacts both charge and spin transport properties. Here the key ingredient is the consideration of the dominant Elliot–Yafet spin relaxation mechanism. The main outcome of this approach is depicted by the dotted lines in Figure 2b,c, where quantitative agreement with the experimental results is achieved. In the following discussion, we introduce this theoretical model.

To develop an accurate description of the channel, we rely on the knowledge of its geometry from TEM imaging (Figure 1). We observe how at the steep walls of the trench the film thickness was reduced, relative to its nominal thickness. This variation in thickness is determined by the e-beam evaporation technique used to grow the film, where nominal thickness is only achieved when the Al beam impinges on the substrate at a normal incidence. With this direct evidence of thickness inhomogeneity, we have incorporated it in our description of the curved channel by modeling the trench profile as a Gaussian bump with fwhm of ≈100 nm, as shown in Figure 3a. The resulting thickness of the Al channel in the local surface normal direction \(\hat{n}\) then becomes intrinsically inhomogeneous. We describe the Gaussian bump as \(h(x) = A \exp(-x^2/\sigma^2)\), where the x coordinate is measured with respect to the maximum trench height position. We next consider that the top surface of the evaporated Al film assumes the same profile with \(h_{l}(x) = t_{0} + h(x)\), and \(t_{0}\) is the nominal thickness. With this, the total volume of the evaporated Al channel does not depend on the geometry of the trench, and it is given by \(t_{0}Lw\), where \(w\) is the channel width and \(L\) the distance in the \(\hat{x}\) coordinate between injector and detector. In order to subsequently derive the local thickness profile, we write the following line element:

\[
ds^2 = \left[ 1 + \left( \frac{dh(x)}{dx} \right)^2 \right] dx^2
\]

which expresses the arclength measured from the injector electrode as

\[
s(x) = \int_{-L/2}^{x} \left[ 1 + \left( \frac{dh(x')}{dx'} \right)^2 \right] dx'
\]

The channel length between injector and detector is given by \(L' = s(L/2)\). Furthermore, the local thickness profile can be obtained by requiring \(\int_{-L/2}^{x} t(s) ds \equiv t_{L}\). This relation is satisfied for a local thickness profile, which in terms of the x coordinate can be expressed as

![Figure 2](image_url)

**Figure 2.** Nonlocal spin valve signal and channel resistance measurements and modeling. (a) Spin valve measurements at \(T = 4.2\) K for devices with different channel geometries. The black arrow indicates the direction of increasing trench height, A. The spin signal ΔR\text{NL} decreases with increasing A. (b) ΔR\text{NL} as a function of A. The experimental data and the modeling result are shown as solid spheres and dotted line, respectively. The shaded region in gray represents the uncertainty due to device to device variation. (c) Experimental data and modeling results for the charge resistance (R) of the channel, for different A.
Figure 3. Geometry-induced tuning of charge resistance and spin resistance. (a) The trench geometry is modeled as a Gaussian bump, and the profile of the Al channel across the trench is mapped out. The trench height \(h\) and the unit vector \(\mathbf{s}\) along the arclength of the Al film, perpendicular to the local surface normal \(\mathbf{n}\), have been illustrated. (b) Calculated variation of the spin relaxation length in Al along \(s\) at 4.2 K. (c,d) 2D color maps illustrating the modulation of charge resistance (c) and spin resistance (d) with the channel geometry, considering a template in the form of a Gaussian bump with height \(A\) and full width at half-maximum \(\sigma\). This, in turn, allows us to find the local behavior of the resistivity \(\rho(t)\). The total charge resistance of the Al channel can be then calculated by using \(R = \int \rho(s) / t(s) w ds\).

A proper modeling of the charge and spin transport properties therefore requires us to explicitly consider the thickness dependence of the resistivity. We do so by employing the Mayadas–Shatzkes (MS) model, which accounts for the increase of electrical resistivity of the thin channel due to electron scattering at grain boundaries. Assuming that the thickness in the local surface normal of the Al channel corresponds to the smallest dimension between grain boundaries, the MS model provides us with a functional form of the resistivity as a function of the thickness:

\[
\rho(t) = \rho_0 \left[ \frac{1}{3} \frac{1}{e(t)} \right] \left[ \frac{1}{2} \frac{1}{e(t)} - \frac{1}{2} \right] \left( \frac{1}{\alpha} \right)
\]

where \(\rho_0\) is the resistivity of bulk Al, and \(\alpha = \lambda/(t(1 - C))\) can be determined from the knowledge of the electronic mean free path, \(\lambda_{\text{e}}\), and the empirical reflectivity coefficient, \(C\). We estimate the latter by using the value of the room-temperature mean free path \(\lambda_{\text{e}} = 18.9\ \text{nm}\) and bulk Al resistivity \(\rho_0 = 2.65 \times 10^{-8}\ \Omega\ \text{m}\),\(^\text{26}\) and our experimental average resistivity at room temperature for reference Al channels of nominal thickness, \(\rho(t_0) = 8.9 \times 10^{-8}\ \Omega\ \text{m}\). We thereby obtain a reflectivity coefficient \(C \approx 0.82\). For the reference devices, we got a device to device statistical variance of \(\approx 2\ \Omega\), of the same size as the symbol for \(A = 0\) in Figure 2c. A statistical variance in the reflectivity coefficient of \(\pm 0.04\) allows us to account for this device to device variation. Considering the scattering related to grain boundaries to be temperature independent, the obtained reflectivity coefficient can be further used to model the thickness dependent resistivity at a low temperature, which we calibrate using our experimental average resistivity for reference channels at 4.2 K, \(\rho(t_0) = 5.6 \times 10^{-8}\ \Omega\ \text{m}\). The values of resistivities considered above are consistent with the range of values observed for thin Al films in previous studies.\(^\text{26}\)

The ensuing behavior of the charge resistance as a function of the trench height fits nicely with our experimental results [c.f., Figure 2c].

To obtain the inhomogeneous profile of the spin relaxation length, we use the fact that the latter can be expressed as \(\lambda = \sqrt{\rho(t)} D\), where \(D\) is the diffusion coefficient and \(\tau_s\) is the spin relaxation time. Using the Einstein relation, \(D = 1/(\rho e^N_{\text{Al}})\), with \(N_{\text{Al}}\) the density of states in the channel at the Fermi level, we can therefore predict the thickness dependence of the diffusion constant. Moreover, the Elliot–Yafet mechanism predicts a scaling of the spin relaxation time, \(\tau_s \propto \tau_{\text{p}} \propto 1/\rho\), where \(\tau_{\text{p}}\) is the momentum relaxation time. These considerations yield \(\lambda \propto \rho^{-1}\), and allow us to consider the ansatz for the thickness dependence of the spin relaxation length \(\lambda(t) = \lambda_0 \rho_0(t)/\rho(t)\), whose functional form is uniquely determined by eq 2, while the unknown \(\lambda_0\) is fixed by requiring the spin relaxation length at the nominal thickness to be equal to that measured in reference devices, \(\lambda_0 = 660\ \text{nm}\) at 4.2 K.\(^\text{26}\)

The ensuing spin relaxation length along the curved Al channel is shown in Figure 3b, with a behavior that is clearly inverse to that of the resistivity.

The spin valve signal is determined by the spin relaxation length and resistivity of the channel, which are both intrinsically inhomogeneous. This intrinsic inhomogeneity impedes the calculation of the spin signal using the simple analytical framework originally introduced by Takahashi and Maekawa for homogeneous channels. For this reason, we have thereby extended the model by fully taking into account the inhomogeneity of the spin relaxation length along the channel [see Supporting Information, sections 2 and 3]. With this approach, we find a closed expression for the spin accumulation signal in the ohmic contact regime, which reads

\[
\Delta R_{\text{NL}} = \frac{4P_0^2}{(1 - P_0^2)^2} \frac{R_{\text{NL}}^2}{R_{\text{N}}^2} \frac{e^{-\lambda_0^2/(1 - P_0^2) d}_{\text{C}}}{1 - e^{-3\lambda_0^2/(1 - P_0^2) d}_{\text{C}}}
\]
where \( w \) is the channel width, \( L' \) is the distance between injector and detector along the arclength \( s \), \( \lambda_s \) is the equal spin relaxation length at the injector and detector, \( R_{NL} = \rho_s \lambda_s / w t_s \), \( R_f \) is the resistance of the ferromagnetic electrode with length \( \lambda_f \) (\( \lambda_f \) being the corresponding spin relaxation length), and \( p_f \) is the current polarization of the ferromagnetic electrodes. The latter two quantities can be obtained from the spin signal in reference flat devices. Therefore, the knowledge of the local behavior of the spin relaxation length allows us to obtain \( \Delta R_{NL} \), as a function of the trench height. For the case of a homogeneous channel, the integral in the exponents simplify to \( L/\lambda_N \) and eq 3 reproduces the usual theory.29 By considering the same statistical variance in the reflectivity coefficient, \( C \), derived from the charge transport above, we find a striking agreement between the theoretical results and the experimental spin valve data, as shown in Figure 2b. The latter serves as experimental validation of our generalized diffusive spin transport model for inhomogeneous channels here presented. This in turn allows us to identify the dominant physical properties controlling spin transport in three-dimensional architectures, where inhomogeneity is directly controlled by the local geometry.

The analytical expression obtained in eq 3 allows us to interrogate in an efficient manner a broader phase space of geometrical variations of curved templates, e.g., as the Gaussian bumps described in Figure 3a,b. The resulting 2D maps for charge resistance and spin resistance, due to the exploration of the phase space of Gaussian bump height \( A \) and full width at half-maximum \( 2 \sqrt{2 \ln 2} \sigma \), are shown in Figure 3c,d. A key observation is the distinct scaling of the charge resistance and the spin resistance due to geometric control, evidenced by the different contour lines in both 2D maps. We highlight this difference by mapping a contour line from each 2D map into the other, resulting in 3D plots shown in Figure 3e,f. Here, we observe the direct tuning of spin resistance independent of the charge resistance, and vice versa, via the nanoscale design of the template geometry. This hitherto unexplored approach to control the ratio of spin resistance to charge resistance, even within a single material system, has the potential to aid in the design of future circuits based on pure spin currents.36

Our curved-template approach enables control of the ratio of spin resistance to charge resistance in individual nanochannels, while allowing the fabrication of a spintronic architecture via a single deposition of the channel material. For flat homogeneous nanochannels, the need of multiple deposition steps for each desired thickness would rapidly lead to an impractical fabrication process. Therefore, it is relevant to consider how simply tuning the length in flat homogeneous nanochannels, which is practical via lithography, compares with curved inhomogeneous nanochannels at the same nominal thickness. For a flat nanochannel to achieve a charge resistance \( R/R_{ref} = 3.0 \), its length must be increased to 3 times that of a reference channel, which leads to a spin resistance \( \Delta R_{NL} / \Delta R_{NL,ref} = 0.17 \). This is significantly lower than the value of up to 0.52 obtained in Figure 3f and is one example of the general advantage offered by curved inhomogeneous channels for efficient individual control of spin and charge resistances [see Supporting Information, sections 4 and 5]. Spatial inhomogeneity below the characteristic scale length for spin transport, \( \text{fwhm} \leq \lambda_s \), combined with control of thickness down to the characteristic length scale for charge transport, \( t \leq \lambda_f \), has been a hitherto unrecognized physical approach to enable such an efficient control within the context of Elliot–Yafet spin relaxation.38,39

Using lateral nonlocal spin valves, we have demonstrated that an appropriate geometric design of metallic nanochannels yields spin resistance changes at constant electrical resistance and vice versa. Although spatially inhomogeneous nanochannels can be created in planar structures,3,8,9 our approach, using three-dimensional nanodevices with a designed curved profile, intrinsically provides the necessary control to achieve the independent tuning of spin and charge resistances. Note that for planar structures there are other methods for controlling spin and charge currents. These rely on novel nanoscale materials, or heterostructures thereof, to gain functionality by active use of electric field,31–34 drift current,35,36 or proximity-induced spin relaxation.37,38 Such methods are highly relevant for current research, though their integration with current technologies is limited by their requirement of novel materials or low temperatures. In contrast, we expect our geometrical approach to be completely generic and thus applicable to other nonmagnetic materials exhibiting a dominant Elliot–Yafet spin relaxation mechanism, e.g., Cu, or heterostructures thereof.3,5,30 The combination of geometrical control and novel nanoscale materials is an interesting avenue for future spintronic technologies.

Recent works have explored technologically relevant curvilinear nanoarchitectures that transport vertically domain walls for magnetologic applications.32,33 Others have used curved templates prestructured via self-assembly of nanostructures, which allows for the nanoscale tuning of the microstructure, thickness, and magnetic anisotropy of the deposited magnetic curved films.39 Geometrical effects can trigger new functionalities both in semiconducting40–44 and superconducting45 low-dimensional systems. The geometrical control of pure spin currents demonstrated in this work can thus inaugurate the search for novel effects in spintronic devices using other ultrathin curved materials like semiconductors and superconductors.

**ASSOCIATED CONTENT**

Supporting Information

The Supporting Information is available free of charge on the ACS Publications website at DOI: 10.1021/acs.nanolett.9b01994.

Additional room-temperature measurements and modeling of pure spin currents in inhomogeneous metallic channels, spin accumulation signal, effect of changing the total thickness and/or the channel length of a flat homogeneous channel, generalized advantage of a curved inhomogeneous nanochannel, and simplified model only considering an increased channel length (PDF)

**AUTHOR INFORMATION**

Corresponding Authors
*E-mail: K.S.Das@rug.nl.
*E-mail: C.Ortix@uu.nl.
*E-mail: ivan.veramarun@manchester.ac.uk.

ORCID
Kumar Sourav Das: 0000-0002-3586-1797
Denys Mäkarov: 0000-0002-7177-4308
Carmine Ortix: 0000-0002-6334-0569
Ivan J. Vera-Marun: 0000-0002-6347-580X
Author Contributions
C.O., P.G., D.M., and I.J.V.M. conceived and supervised the project. I.J.V.M. and K.S.D. conceived and designed the experiments. K.S.D. carried out the experiments and the initial data analysis. D.M. supplied the curved templates and the corresponding electron microscopy imaging. C.O. developed and performed the theoretical analysis with the help of P.G. and M.C. K.S.D., C.O., and I.J.V.M. performed the final data analysis and wrote the manuscript with the help of B.J.v.W., M.C., P.G., and D.M. All authors discussed the results and the manuscript.

Notes
The authors declare no competing financial interest.

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